

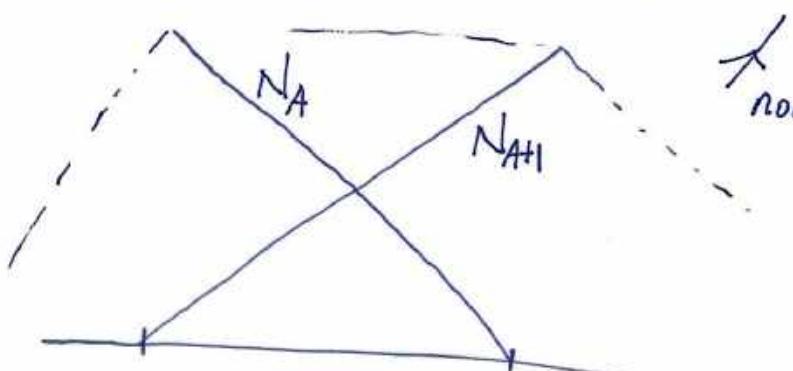
Element / local point of view

Observation : $N_A = 0$ outside of a neighborhood of node A.

→ We only need to consider the neighborhood of node A when performing integration involving N_A .
 Simplify the computer implementation.

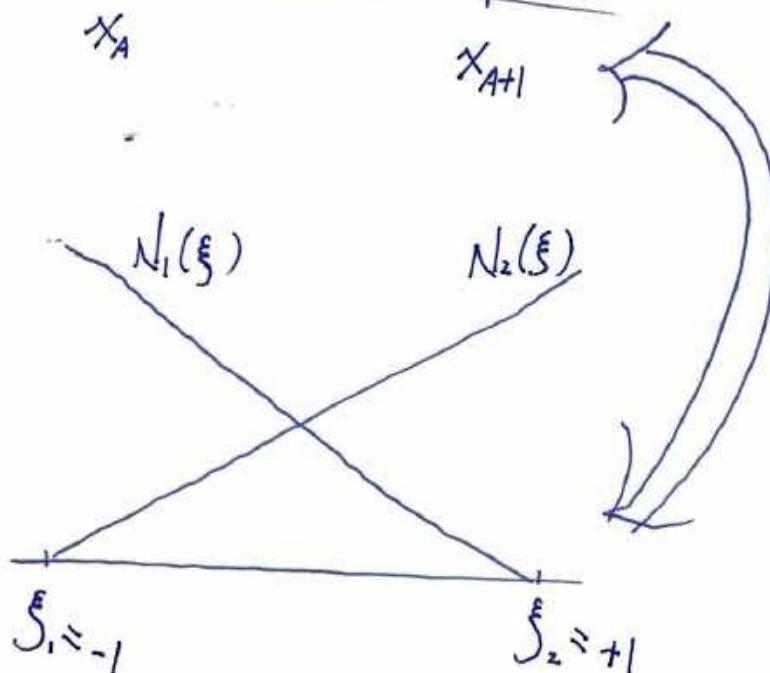
We shall restrict ourselves to 1D linear element and we will generalize the idea to multi-D and higher-order later.

Recall in the 1D element $[x_A, x_{A+1}]$



$$u^h = N_A d_A + N_{A+1} d_{A+1}$$

for $x \in [x_A, x_{A+1}]$.



$$x = x(\xi) = \frac{\xi h_A + x_A + x_{A+1}}{2}$$

$$\xi = \xi(x) = \frac{2x - x_A - x_{A+1}}{h_A}$$

$$N_1 = \frac{1-\xi}{2}$$

$$N_2 = \frac{1+\xi}{2}$$

or $N_a(\xi) = \frac{1+\xi_a \xi}{2}$

$$\text{Verify that: } 1) N_A(x) = \underset{\parallel}{N}_A \circ \xi(x) \quad N_{A+1}(x) = \underset{\parallel}{N}_2 \circ \xi(x)$$

$$2) x(\xi) = \underset{\parallel}{x}_1^e N_1(\xi) + \underset{\parallel}{x}_2^e N_2(\xi).$$

$$K = a(N_A, N_B) = \int_0^1 N_{A,x} N_{B,x} dx = \sum_{e=1}^{n_{el}} \int_{\Omega_e} N_{A,x} N_{B,x} dx$$

$$= \sum_{e=1}^{n_{el}} K^e \quad \text{with } K^e = \left[\int_{\Omega_e} N_{A,x} N_{B,x} dx \right].$$

Stiff with size $n_{eq} \times n_{eq}$, K^e has non-zero entries only for N_A, N_B has support in Ω_e .

For 1D linear element:

in $\Omega^e = [x_c, x_{c+1}]$ we only need to consider $A = c, c+1$
 $B = c, c+1$.

$$x^e = \begin{bmatrix} K_{ab}^e \end{bmatrix}_{2 \times 2} \quad K_{ab}^e = \int_{\Omega^e} \underset{1,2}{N_{a,x}} \underset{1,2}{N_{b,x}} dx$$

$$= \int_{-1}^1 N_{a,\xi} \frac{\partial \xi}{\partial x} N_{b,\xi} \frac{\partial \xi}{\partial x} \frac{\partial x}{\partial \xi} d\xi$$

1D change of variable formula

$$\int_{x_1}^{x_2} f(x) dx = \int_{\xi_1}^{\xi_2} f(x(\xi)) x_{,\xi}(\xi) d\xi$$

if $x: [\xi_1, \xi_2] \rightarrow [x_1, x_2]$ is differentiable

$$= \int_{-1}^1 N_{a,\xi} N_{b,\xi} \frac{\partial \xi}{\partial x} d\xi$$

$$= \int_{-1}^1 \frac{\xi_a}{2} \frac{\xi_b}{2} \frac{2}{h_A} d\xi$$

$$= \frac{\xi_a \xi_b}{2 h_A}$$

$$= \frac{(-1)^{a+b}}{h_A}$$

$$K^e = \begin{bmatrix} \frac{1}{h_A} & -\frac{1}{h_A} \\ -\frac{1}{h_A} & \frac{1}{h_A} \end{bmatrix}$$

$$K = \begin{bmatrix} \frac{1}{h_1} & -\frac{1}{h_1} & & & & & & \\ -\frac{1}{h_1} & \frac{1}{h_1} + \frac{1}{h_2} & -\frac{1}{h_2} & & & & & \\ & & & \ddots & & & & \\ & & & & \boxed{-\frac{1}{h_{A-1}} & \frac{1}{h_{A-1}} + \frac{1}{h_A} & -\frac{1}{h_A}} & & & \\ & & & & & \boxed{\frac{1}{h_A} & \frac{1}{h_A} + \frac{1}{h_{A+1}} & -\frac{1}{h_{A+1}}} & & & \\ & & & & & & \ddots & & \\ & & & & & & & \frac{1}{h_{n-1}} & \frac{1}{h_{n-1}} \end{bmatrix}$$

Two data structures:

$IEN(a, e) = A$

global node number

\nearrow local node number
 \searrow element number

$$LM(a, e) = ID(IEN(a, e)).$$

Summary: In each element, there are n_{en} nodes / nonzero basis functions. We may denote them as $\{N_a\}_{a=1}^{n_{\text{en}}}$, and it is often convenient to pull them back onto a referential element, on which $N_a = N_a(\xi)$ with the mapping $\xi = \xi(x)$.

On each element, we may build a small matrix K^e , known as the element / local stiffness matrix.

$$K^e = [K_{ab}^e] \quad K_{ab}^e = a(N_a, N_b).$$

and

$$K_{PQ} \leftarrow K_{PQ} + K_{ab}^e \quad P = LM(a, e) \neq 0 \\ Q = LM(b, e) \neq 0.$$

Σ
adding the contribution of element e .

For the load vector

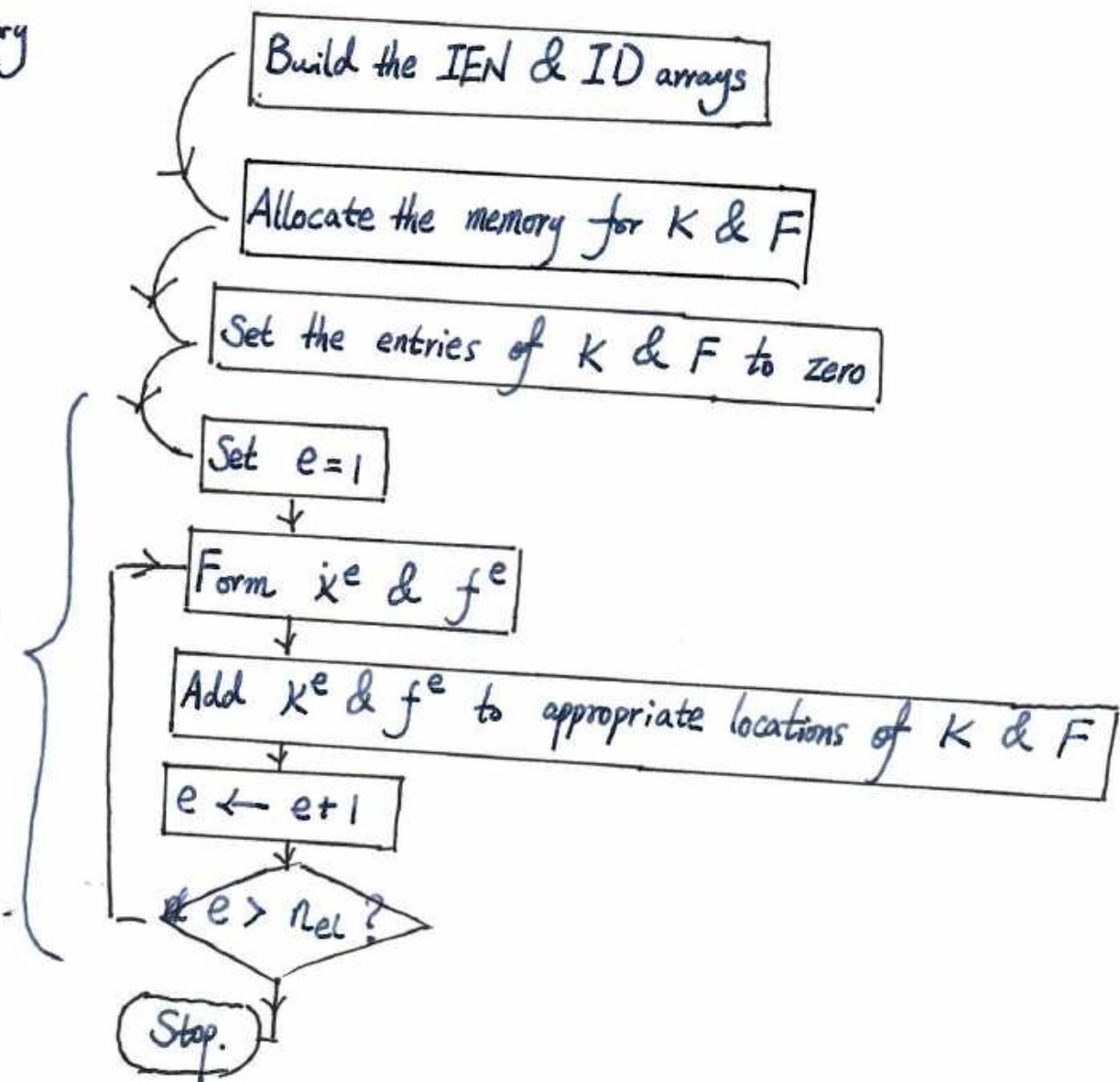
$$F = \sum_{e=1}^{n_{\text{el}}} F^e = \sum_{e=1}^{n_{\text{el}}} \left\{ (N_A, f)^e + (N_A, g)_R^e - a(N_A, N_B)g_B^e \right\}$$

$$f_a^e = \int_{\Omega_e} N_a f \, d\Omega + \int_{\Gamma_e} N_a h \, d\gamma - \sum_{b=1}^{N_e} K_{ab}^e g_b^e$$

$g_b^e = g(x_b^e)$ if g
is prescribed at x_b^e , otherwise 0.

Summary

Assembly
algorithm
denoted as
 A



$$K = \bigcup_{e=1}^{N_e} K^e \quad \& \quad F = \bigcup_{e=1}^{N_e} f^e$$

Constructing the element stiffness matrix & load vector

We gained our first experience in the local/element assembly from the 1D example, in which we applied the chain rule and change-of-variable formula. In multi-dimensional cases, we need to generalize the two and introduce the concept of quadrature.

1. Quadrature.

Let $f: \Omega^e \subset \mathbb{R}^{n_{sd}} \rightarrow \mathbb{R}$ be given, we are interested in computing $\int_{\Omega^e} f(x) d\Omega$.

We always pull the integrand back to the referential/parent element,

$$n_{sd}=1 : \int_{\Omega^e} f(x) dx = \int_{-1}^1 f(x(\xi)) x_{,\xi}(\xi) d\xi$$

$$n_{sd}=2 : \int_{\Omega^e} f(x, y) d\Omega = \int_{-1}^1 \int_{-1}^1 f(x(\xi, \eta), y(\xi, \eta)) j(\xi, \eta) d\xi d\eta$$

$n_{sd}=3$ is analogous to the case of $n_{sd}=2$. Refer to p. 140.

We only need to design an approach for numerical integration over the 'fixed' parent elements.

$j = \det \left[\frac{\partial x}{\partial \xi} \right]$,
the Jacobian determinant.

For $n_{\text{sd}} = 1$ $\int_{-1}^1 f(\xi) d\xi = \sum_{e=1}^{n_{\text{int}}} f(\tilde{\xi}_e) w_e + R$ remainder.

$\underbrace{\text{number of quadrature points}}_{\approx} \sum_{e=1}^{n_{\text{int}}} f(\tilde{\xi}_e) w_e$ $\underbrace{\text{e-th weight}}$

$\underbrace{\text{coordinate of the e-th quadrature pt}}$

e.g. $n_{\text{int}} = 1$, $\tilde{\xi}_1 = 0$, $w_1 = 2$, $R = \frac{f(\xi)(\bar{\xi})}{3}$

$n_{\text{int}} = 2$, $\tilde{\xi}_1 = -\frac{1}{\sqrt{3}}$ $w_1 = 1$
 $\tilde{\xi}_2 = \frac{1}{\sqrt{3}}$ $w_2 = 1$ $R = \frac{f^{(4)}(\bar{\xi})}{135}$

$$\int_{-1}^1 \int_{-1}^1 f(\xi, \eta) d\xi d\eta \approx \sum_{\ell^{(1)}=1}^{n_{\text{int}}^{(1)}} \sum_{\ell^{(2)}=1}^{n_{\text{int}}^{(2)}} f(\tilde{\xi}_{\ell^{(1)}}, \tilde{\eta}_{\ell^{(2)}}) w_{\ell^{(1)}}^{(1)} w_{\ell^{(2)}}^{(2)}$$

$$= \sum_{e=1}^{n_{\text{int}}} f(\tilde{\xi}_e, \tilde{\eta}_e) w_e.$$

2. Shape function subroutines

Chain rule : $N_{a,x} = N_{a,\xi} \underline{\xi}_{,x} + N_{a,\eta} \underline{\eta}_{,x}$ ($n_{sd}=2$)

$$N_{a,y} = N_{a,\xi} \underline{\xi}_{,y} + N_{a,\eta} \underline{\eta}_{,y}$$

Isoparametric element : Let $x: \widehat{\Omega} \rightarrow \Omega^e$ be of the form

$$x(\xi) = \sum_{a=1}^{n_{en}} N_a(\xi) x_a^e$$

and if the local interpolation function is of the

$$u^h(\xi) = \sum_{a=1}^{n_{en}} N_a(\xi) u_a^e$$

the element is isoparametric.

If the element is isoparametric, we have

$$x(\xi, \eta) = \sum_{a=1}^{n_{en}} N_a(\xi, \eta) x_a^e$$

$$y(\xi, \eta) = \sum_{a=1}^{n_{en}} N_a(\xi, \eta) y_a^e$$

$$\begin{aligned} \rightarrow x_{,\xi} &= \sum_{a=1}^{n_{en}} N_{a,\xi}(\xi, \eta) x_a^e & \left[\begin{array}{cc} \frac{\partial \xi}{\partial x} & \frac{\partial \xi}{\partial y} \\ \frac{\partial \eta}{\partial x} & \frac{\partial \eta}{\partial y} \end{array} \right] \\ x_{,\eta} &= \cdots N_{a,\eta} \cdots \cdots \end{aligned}$$

$$y_{,\xi} = \cdots N_{a,\xi} \cdots y_a^e = \begin{bmatrix} x_{,\xi} & x_{,\eta} \end{bmatrix}^{-1}$$

$$y_{,\eta} = \cdots N_{a,\eta} \cdots y_a^e = \begin{bmatrix} y_{,\xi} & y_{,\eta} \end{bmatrix}$$

Cramer's rule:

$$\begin{bmatrix} x_{,S} & x_{,N} \\ y_{,S} & y_{,N} \end{bmatrix}^{-1} = \frac{1}{j} \begin{bmatrix} y_{,N} & -x_{,N} \\ -y_{,S} & x_{,S} \end{bmatrix}$$

$$j = \det \begin{bmatrix} x_{,S} & x_{,N} \\ y_{,S} & y_{,N} \end{bmatrix} = x_{,S} y_{,N} - x_{,N} y_{,S}.$$

Now, the step of forming K^e & f^e can be detailed as.

For $l = 1, \dots, n_{int}$

Form K^e & f^e : Determine ξ_e, η_e, w_e

From
Calculate $x_{,S}(\xi_e, \eta_e), x_{,N}(\xi_e, \eta_e)$
 $y_{,S}(\xi_e, \eta_e), y_{,N}(\xi_e, \eta_e)$.

Calculate $j(\xi_e, \eta_e)$

Calculate $N_{a,x}(\xi_e, \eta_e) \quad N_{a,y}(\xi_e, \eta_e)$.

Calculate K_{ab}^e & f_a^e

End-for-loop

Reference: • Ch. 3.8 & 3.9 Hughes book.

• github.com/M3C-Lab/FEM-1D-demo.